

## [54] SIDELOOKING LASER ALTIMETER FOR A FLIGHT SIMULATOR

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[21] Appl. No.: 234,224

[22] Filed: Feb. 13, 1981

[51] Int. Cl.<sup>3</sup> ..... G01C 3/10; G09B 9/08

[52] U.S. Cl. ..... 356/1; 356/4; 358/104; 358/109; 434/4; 434/38

[58] Field of Search ..... 434/4, 38; 356/1, 4; 358/109, 104

## [56] References Cited

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Primary Examiner—S. C. Buczinski

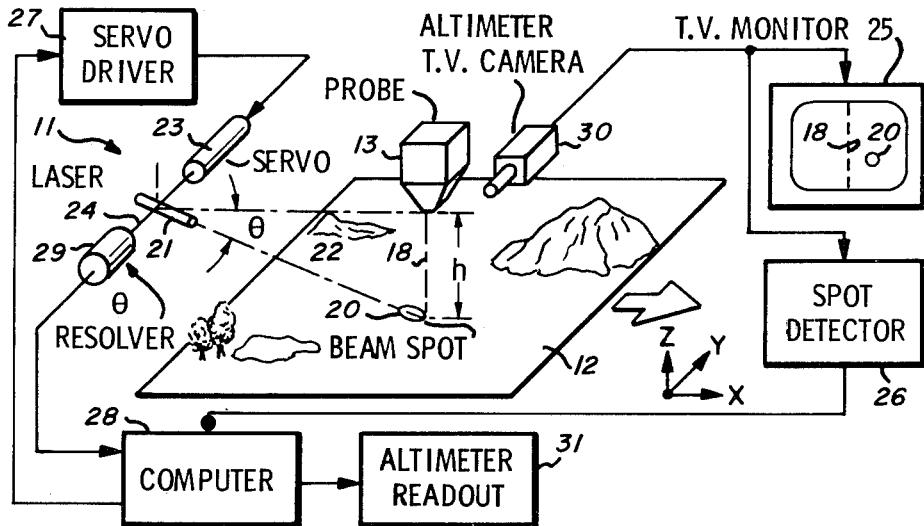
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## [57] ABSTRACT

The object of the invention is to provide an improved laser altimeter for a flight simulator which will allow measurement of the height of the simulator probe above the terrain directly below the probe tip.

A laser beam 22 is directed from the probe 13 at an angle  $\theta$  to the horizontal to produce a beam spot 20 on the terrain. The angle  $\theta$  that the laser beam 22 makes with the horizontal is varied so as to bring the beam spot into coincidence with a plumb line 18 coaxial with the longitudinal axis of the probe 13. A television altimeter camera 30 observes the beam spot and has a raster line aligned with the plumb line 18. Spot detector circuit 26 coupled to the output of the TV camera monitors the position of the beam spot relative to the plumb line 18. An error signal is produced by computer 28 driving, via a servo motor 23, the laser beam optics so as to cause the beam spot to come into coincidence with the plumb line 18. At coincidence, computer 28 looks up in a table the altitude of the probe for the given angle  $\theta$  and reads out the altitude to an altimeter readout 31.

11 Claims, 9 Drawing Figures



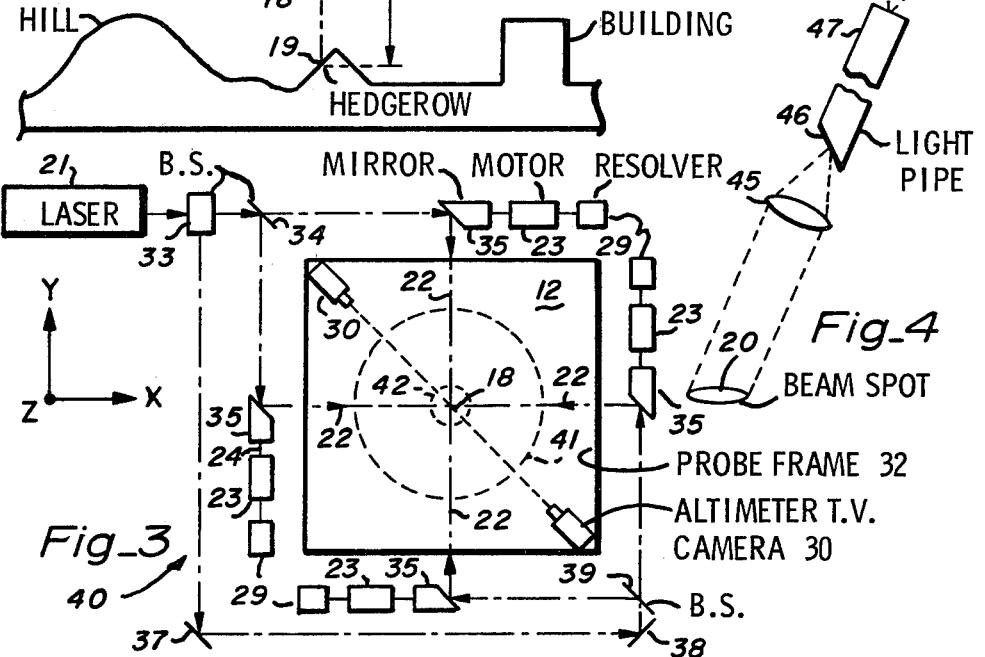
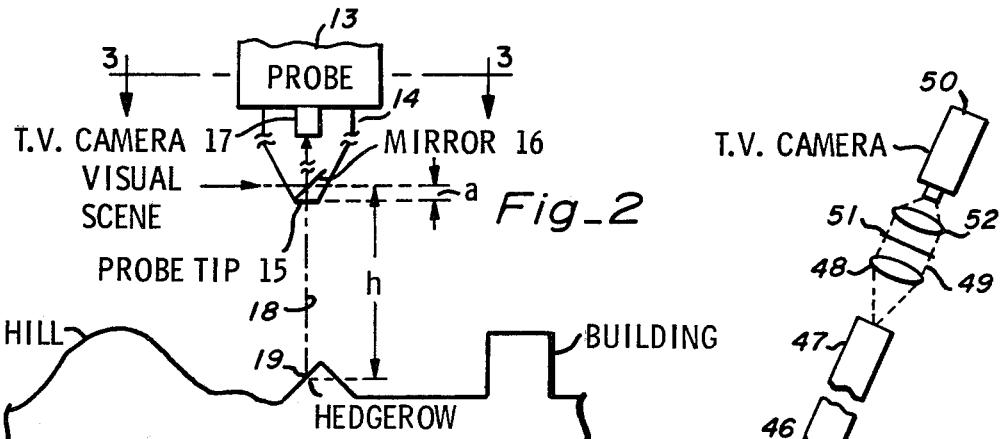
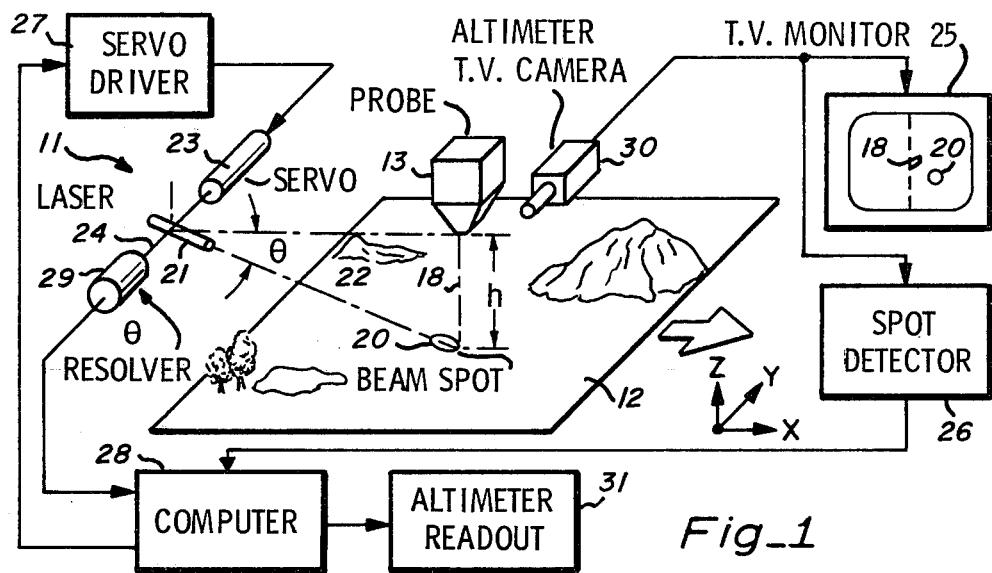


Fig. 4

BEAM SPOT  
PROBE FRAME 32  
ALTIMETER T.V.  
CAMERA 30

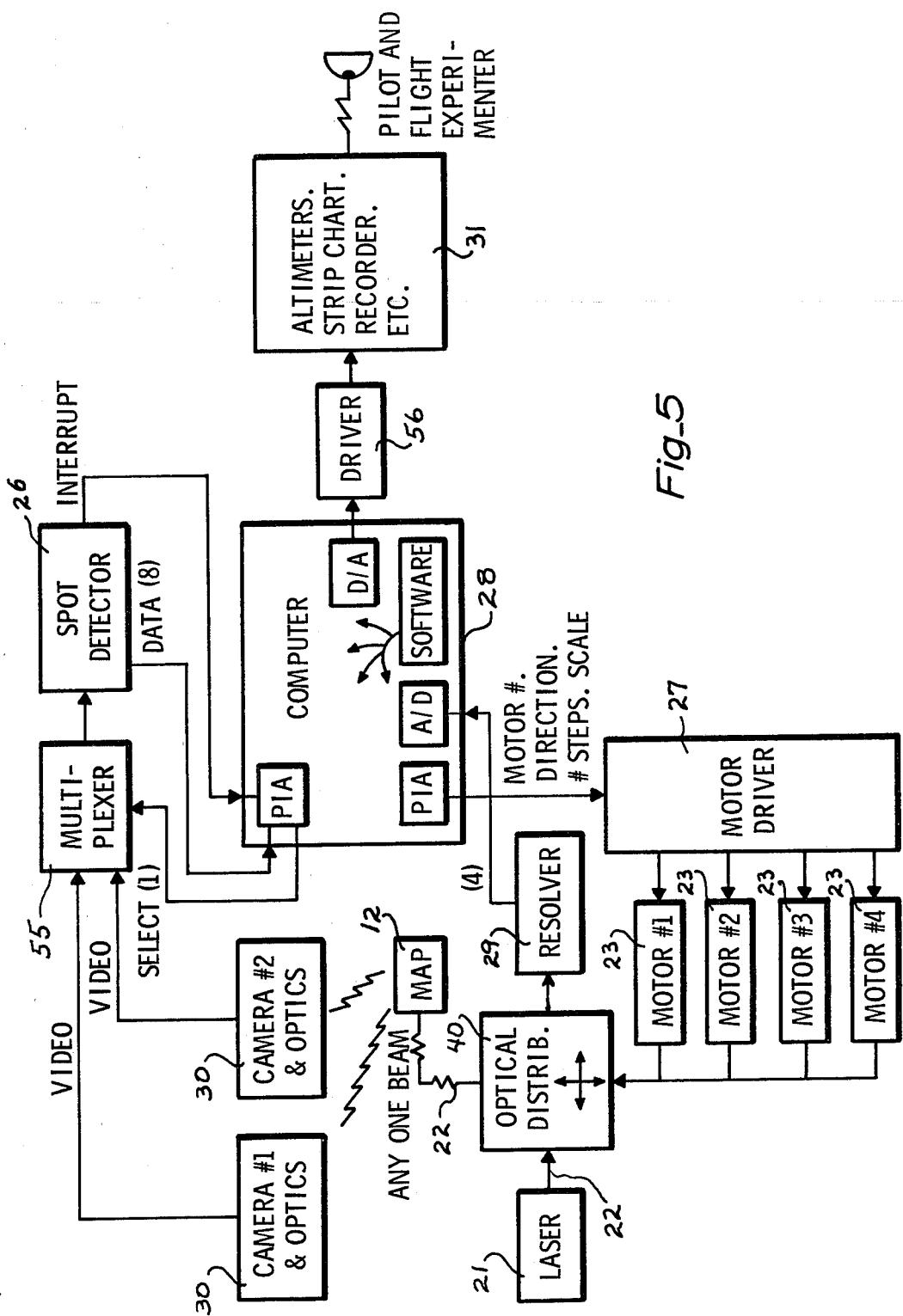


Fig. 5

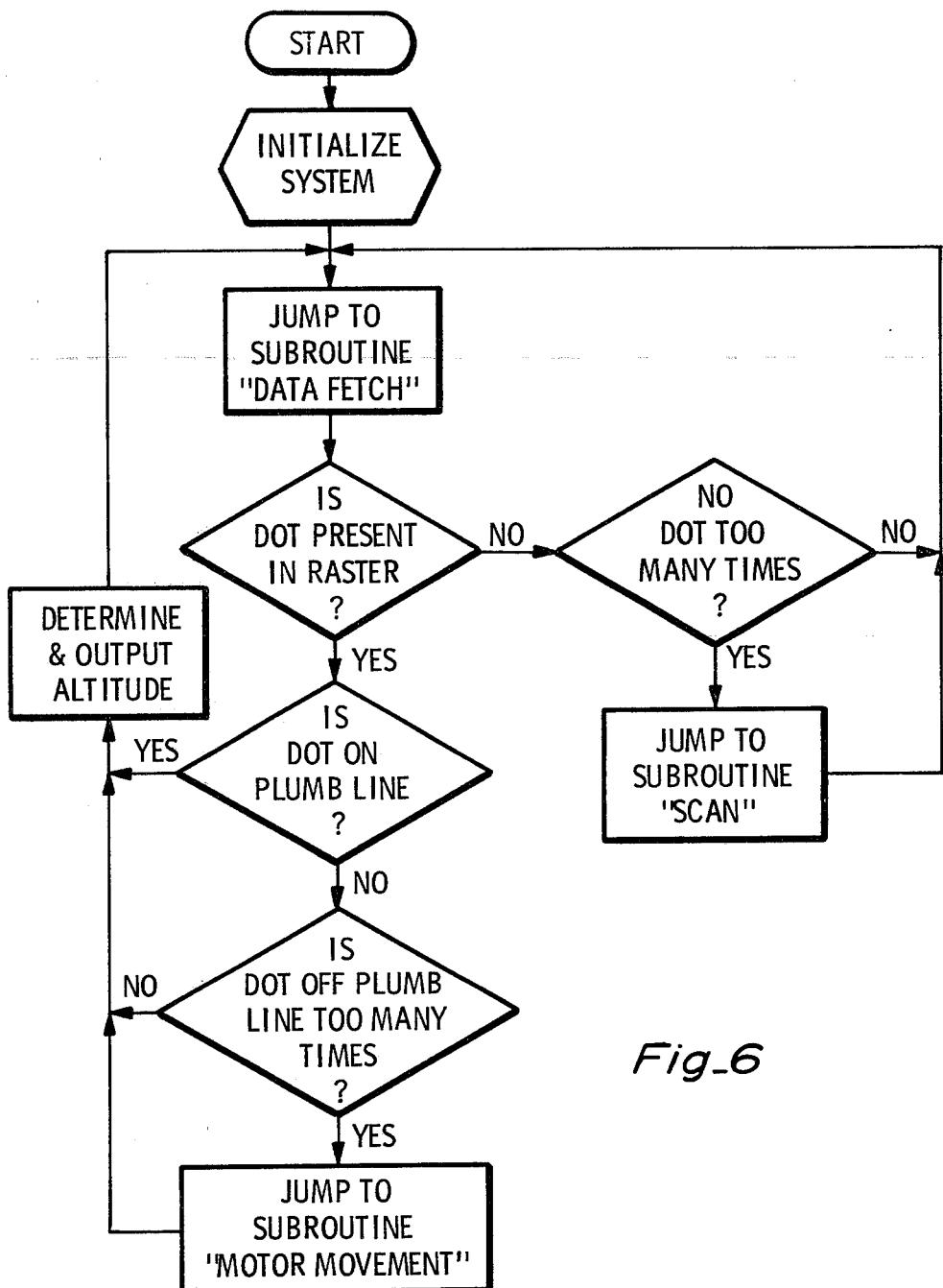


Fig-6

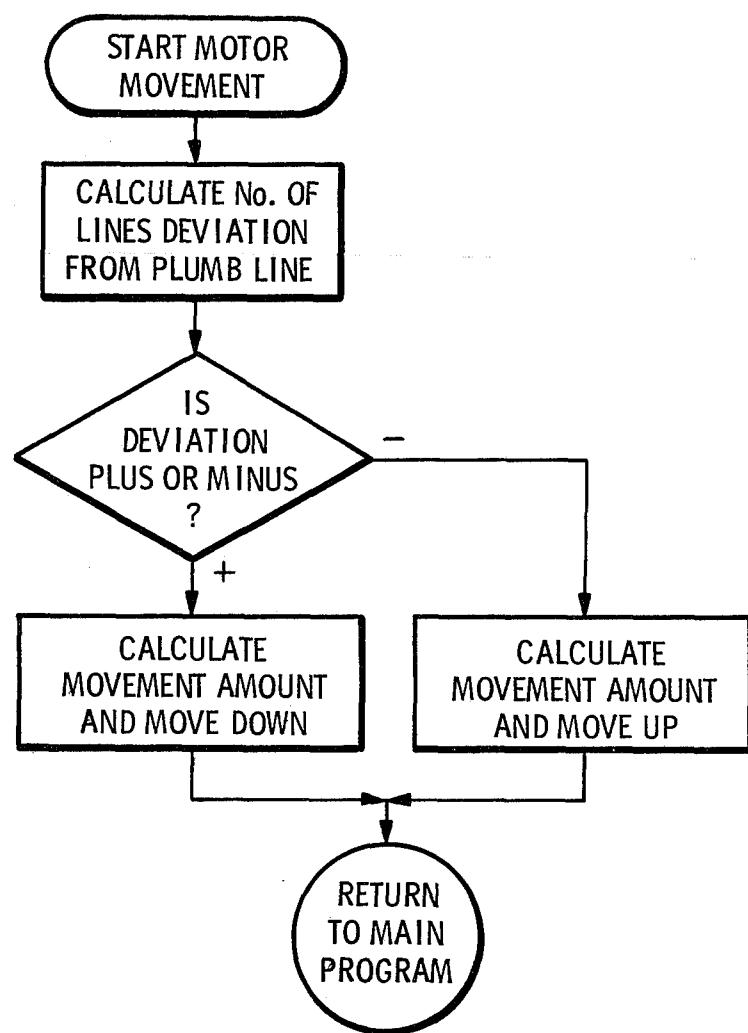


Fig-7

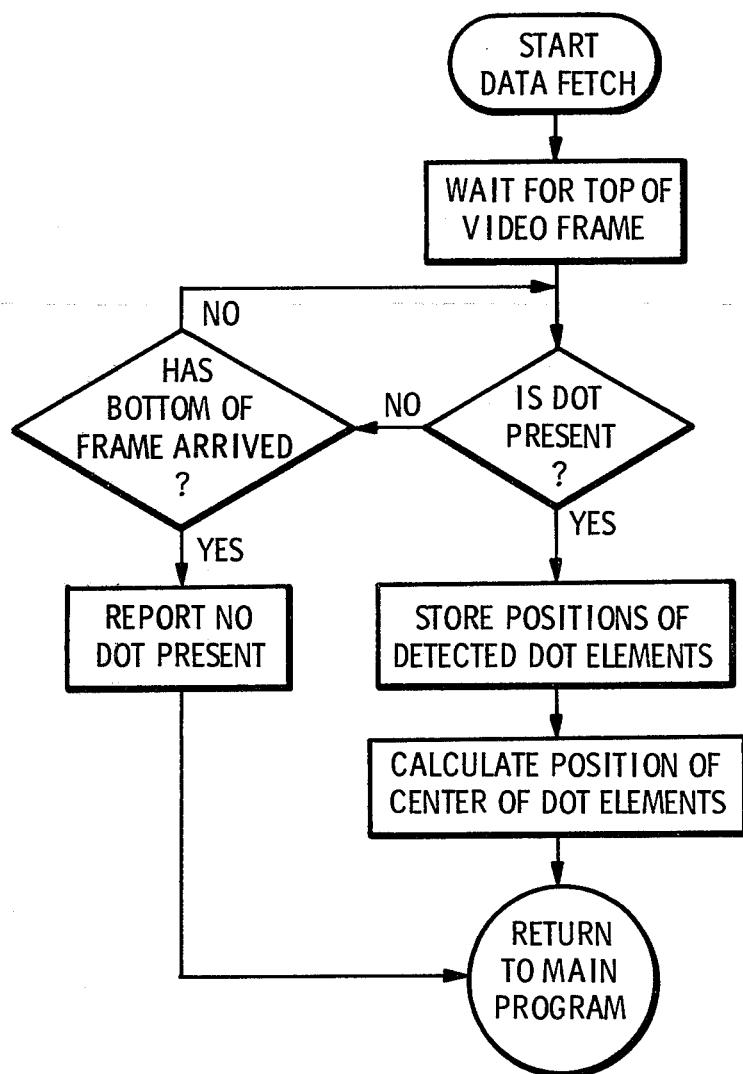
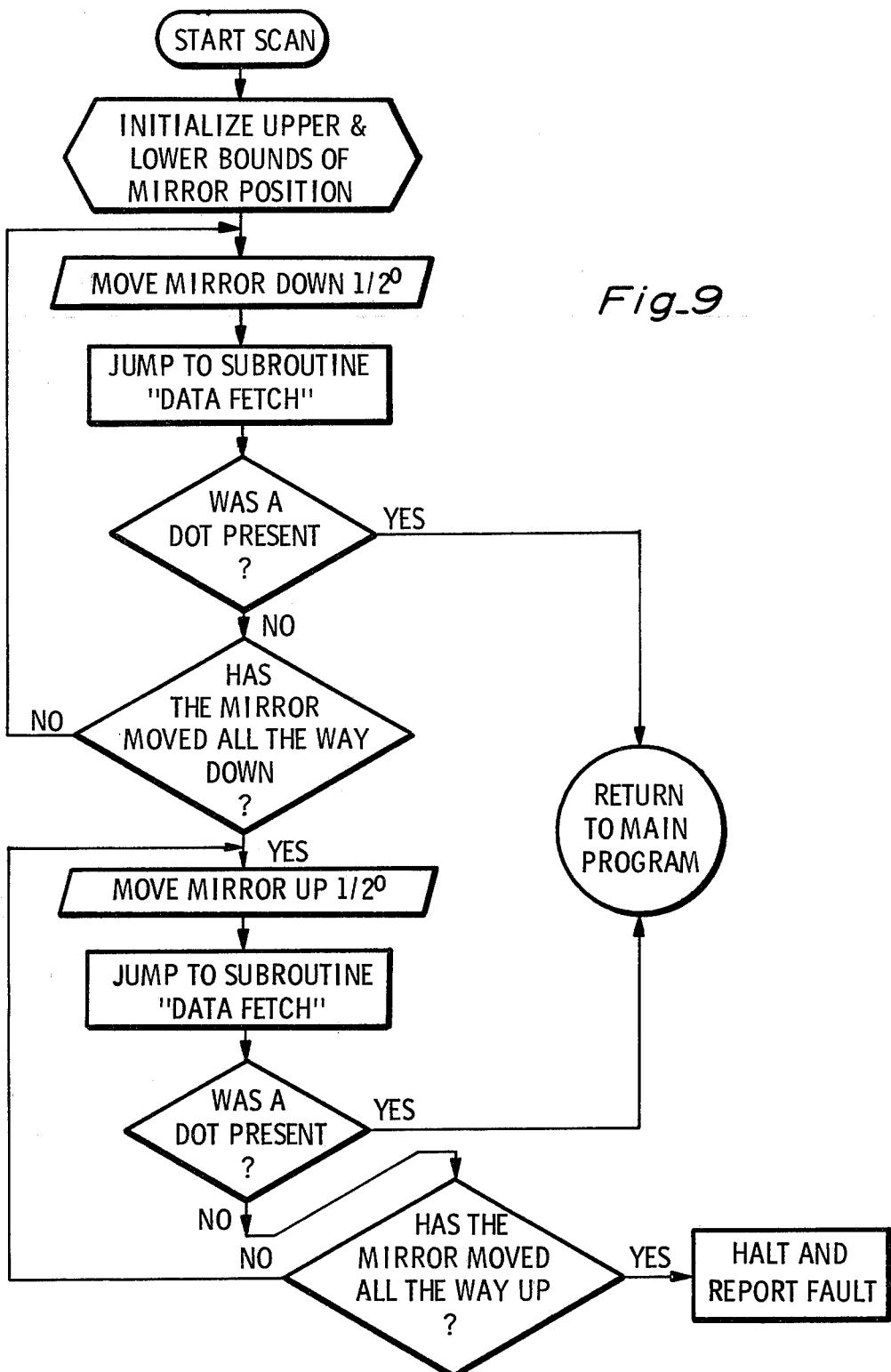


Fig. 8



## SIDELOOKING LASER ALTIMETER FOR A FLIGHT SIMULATOR

### ORIGIN OF THE INVENTION

The invention described herein was made by an employee of the U.S. Government and may be manufactured and used by or for the Government for Governmental purposes without the payment of any royalties thereon or therefor.

### TECHNICAL FIELD

The technical field of the present invention relates in general to laser altimeters for flight simulators.

### BACKGROUND ART

Heretofore a laser altimeter system has been proposed for determining the altitude of a flight simulation probe over a model board. Such a prior art system is disclosed in an article entitled, "Probe Protection In Camera/Model Visual Systems" appearing in the Proceedings of the 1980 Summer Computer Simulation Conference, Olympic Hotel, Seattle, Wash., Aug. 25-27, 1980.

In this system, a laser beam is directed vertically from the flight simulator TV camera probe along a side of the probe to strike a point on the model board radially displaced from a point directly below the center line of the probe, hereafter referred to as a plumb line. The incident beam produces a beam spot on the terrain of the model which is thence imaged onto a linear array sensor. As the height of the probe is varied, while holding the probe otherwise stationary, from a point of minimum altitude to a point of maximum altitude the beam spot traverses a vertical imaginary line focused onto the linear array sensor. The position of the imaged beam spot along the linear array sensor is representative of altitude. A major problem with this system is that the altitude being measured is not the altitude of the probe (altitude measured along the plumb line) but rather the altitude of the laser beam source which is displaced horizontally from the probe. The actual distance between the plumb line and the laser beam must be multiplied by the scale of the model. Error will be produced whenever the terrain elevation at the plumb line differs from the terrain elevation at the laser beam. For example, an appreciable error would exist if the plumb line was over a depression and the laser beam impinged on a hill, mountain or tall building.

Thus, it is desirable to obtain a probe height sensor which more accurately measures the height of the probe above the terrain directly below the probe.

### [STATEMENT OF INVENTION]

### DISCLOSURE OF INVENTION

In the present invention, pilot altitude as represented by the distance  $h$  is measured by a technique that locates the point of intersection of the plumb line and the terrain (hereinafter known as the convergence point). A laser beam is directed from the probe at an angle to the plumb line and coaxial with the longitudinal axis of the probe. The point where the beam strikes the terrain is varied by changing the angle of the laser beam relative to the longitudinal axis of the probe so that the beam spot is brought to a point on the longitudinal axis of the probe where it intersects the terrain. A TV camera, carried from the probe views the region below the probe and has a predetermined linear detection region,

such as a raster line, coaxially aligned with the image of the plumb line. A detection circuit receives the output of the TV camera and determines the position of the laser dot in the raster. Using this information, a computer determines the position of the beam spot relative to the plumb line. A resolver coupled to the laser beam angle control reads out the angular position  $\theta$  of the laser beam to a computer. The computer looks up the height of the probe in a look up table for the angle  $\theta$  of the laser beam. The measured height is then read out to an altimeter and to a flight simulation monitor station. If the laser dot does not reside on the plumb line, a computer directs a stepper motor to relocate the beam such that the dot will reside on the plumb line. If the operative laser beam is unable to be relocated at the convergence point because it is blocked by a terrain obstruction, an alternative laser beam at a different angle around the probe is selected. Also, if the TV camera's view is blocked the computer selects an alternative TV camera.

### BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic perspective view, partly in block diagram form, of an altimeter system for a flight simulator incorporating features of the present invention,

FIG. 2 is a longitudinal sectional view of the flight simulator probe and model board,

FIG. 3 is a schematic transverse sectional view, partly in block diagram form, of a portion of the structure of FIG. 2 taken along line 3-3 in the direction of the arrows,

FIG. 4 is a schematic side elevational view of the TV camera optics for beam spot detection,

FIG. 5 is a schematic block diagram of a laser altimeter system incorporating features of the present invention,

FIG. 6 is a logic flow diagram for the computer program for the system of the present invention, and

FIGS. 7, 8, and 9 are logic flow diagrams for subroutines of the computer program flow diagram depicted in FIG. 6.

### DETAILED DESCRIPTION OF THE INVENTION

Referring now to FIG. 1 there is shown a laser altimeter system 11 for a flight simulator and incorporating features of the present invention. The flight simulator system includes a model board 12 comprising a scale model of terrain over which simulated flights are to be conducted. The pilot sits in a cockpit, not shown, and views a television screen displaying a view seen through a probe 13 movable with respect to the terrain of the model board 12 in accordance with flight control commands given by the pilot over the aircraft controls. The probe 13 is carried from a gantry, not shown, disposed over the terrain of the model board 12. Relative movement in three orthogonal directions, X, Y, and Z is obtained between the probe and the model board. In some embodiments, the gantry moves relative to a stationary model board to provide movement in all three orthogonal directions, whereas, in other embodiments the model board is moved relative to the probe to simulate flight.

Referring now to FIG. 2, the optical system for the probe 13 is shown in greater detail. More particularly, the probe 13 includes an elongated barrel portion 14

projecting in the Z direction toward the model board. At the end or tip of the probe 15 there is a mirror 16 which projects a visual scene corresponding to that which would be seen by the pilot, up along the longitudinal axis of the probe barrel 14 to a TV camera 17. The scene picked up by the TV camera is then transmitted to and displayed on a cathode ray tube outside the windshield of the simulated aircraft. The altitude  $h$  of the simulated aircraft is that scale distance from the mirror 16 is taken along a plumb line 18 for the modeled terrain to a point of intersection of the plumb line with the terrain at 19.

Referring again to FIG. 1, a laser 21 is carried from a frame coupled to and movable with the probe 13. The laser directs a pencil-like beam 22 of monochromatic nondivergent radiation of visible wavelength onto the terrain below the probe 13 having been deflected by pitchable mirror 35 to produce a beam spot 20 on the terrain. A servo motor 23 is coupled to the mirror 35 in such a way as to vary the angle  $\theta$  that the laser beam makes to the horizontal or XY plane of the model board 12. The laser beam is rotatable about an axis of revolution parallel to the horizontal XY plane and such beam being rotatable in a plane normal to said axis of revolution, such plane also containing the plumb line 18.

An altimeter TV camera optical system 30 is also carried from the probe frame. The altimeter TV camera system 30 includes some optics, not shown, and views the region of the model board directly below the probe 13. The TV camera optics are such that the point of intersection of plumb line 18 with the model board surface is within the view of the TV camera system 30 for all values of altitude  $h$  from minimum to maximum above the surface of the model board 12.

A single raster line is made coincident with the plumb line 18 through appropriate mechanical alignment. An output from the altimeter TV camera 30 goes to a spot detector circuit 26 of the type similar to that disclosed in U.S. Pat. No. 3,320,360 issued May 16, 1967 entitled, "Television Tracking Error Detector", for determination of the location of the beam spot 20 relative to the plumb line 18.

The output of spot detector 26 is fed to a computer 28. This output consists of the raster line number and displacement along the raster line of all of the detected elements of the laser spot 20. The computer determines the location of the center of the laser spot 20 in the raster of the altimeter TV camera system 30. To be coincident with the end of the plumb line 18, the laser spot 20 must lie somewhere along the altimeter TV camera system raster line which was made coincident with the plumb line 18. The computer 28 compares the raster line number of the center of the laser spot 20 with the raster line number of the raster line which is coincident with the plumb line 18. If the two are equal then the laser spot 20 must be located on the terrain at the end of plumb line 18 where it intersects the terrain. The exact length of plumb line 18 may then be determined. If the two are not equal, the laser spot 20 is not located at the end of plumb line 18 where it intersects the terrain. An error signal is generated which causes servo driver 27 to reposition laser spot 20 until the two raster line numbers are equal. The computer 28 also receives the angle  $\theta$  input from a resolver 29 mechanically coupled to the laser beam deflection system so that at the point of convergence of the beam spot 20 with the point of entry of the plumb line 18 into the terrain, the computer reads the  $\theta$  angle and looks up, in its look up table,

the value of altitude corresponding to the given values of altitude for various values of  $\theta$  as the probe is moved from a position of minimum altitude to maximum altitude over the model board.

Referring now to FIG. 3 there is shown the optical distribution system for deriving the various laser beams and for televising the beam spot 20 on the model board. The laser 21 is affixed to a probe frame member 32, and directs its output beam through first and second beam splitters 33 and 34. Beam splitter 33 is arranged to direct the reflected portion of the beam downward along the Z axis whereas the other half of the beam passes through the first beam splitter 33, to the second beam splitter 34 which serves to further divide the beam into a first beam directed parallel to the X axis and a second beam of equal amplitude directed along the Y axis. Each of the beams outputted from the second beam splitter 34 is directed onto a 45° angle mirror 35 for bending the respective beam by 90° toward the plumb line 18. Each of the mirrors is driven from a stepping servo motor 23 about respective axes of revolution. In one instance the axis of revolution is parallel to the X axis and in the other to the Y axis and both are in the XY plane so as to cause the beams to be rotated within respective planes 25 which are perpendicular to the XY plane and each of which includes the plumb line 18. A  $\theta$  angle resolver 29 is coupled to each of the motor-mirror drive trains for giving an output determinative of the angle  $\theta$ .

The other half of the output of the first beam splitting mirror 33 is directed downward along the Z axis to a 45° mirror, not shown, which thence directs the beam parallel to the Y axis to a second 45° mirror 37 and thence parallel to the X axis to another 45° mirror 38 which thence directs the beam through a second beam splitting mirror 39 for splitting the beam into two equal components, one parallel to the Y axis and the other parallel to the X axis. The beams are then reflected off of respective 45° mirrors 35 driven from the stepping motors 23 which include resolvers 29. Thus, the second beam produces a pair of beams directed onto the model board 12 which are orthogonal to each other and which are 180° displaced from the first pair of beams. The beams are rotatable in the XZ and YZ planes, such planes each including the plumb line 18. The respective mirrors 35 are positioned such that their output beams will intersect the plumb line 18 at the point that the plumb line 18 intersects the surface of the model 12.

The orthogonality between each of the laser beams is not a requirement. For example, it could be three beams at 120° angular spacing from each other with the camera optics similarly angularly separated from each other by 120° and being spaced at 60° angles from each of the respective beams.

A pair of altimeter TV camera optics are carried from the probe frame structure 32 and are positioned at 180° intervals about an axis of revolution coaxial with the plumb line 18 and preferably at 45° angular spacing from the ZX or ZY planes but on the XY plane containing the respective laser beams. This positioning of the altimeter TV camera optics 30 permits viewing of the respective beam spot 20 at the plumb line 18, regardless of various buildings, hills, or trees or other obstructions in the terrain of the model board 12. In other words there is some combination of laser beam 22 and altimeter TV camera optics 30 which will permit viewing of the beam spot 20 at the plumb line 18 regardless of the obstructions represented by the terrain of the model 12, with the exception of a well or deep ravine. The laser

beams 22 which are not in use, i.e., three of the four are "parked" by rotating their respective mirrors 35 so as to project the beam spot 20 onto the probe body 41 or 42.

Referring now to FIG. 4 there is shown one of the optical systems 30 for each of the TV altimeter cameras. More particularly, a condensing lens 45 receives the light emanating from the beam spot 20 and focuses the image of the beam spot onto the entrance plane 46 of a light pipe 47 such as a fiber optics bundle. The bundle 47 may have a suitable length as of 3-5 feet to bring the image of the beam spot 20 to a convenient location of the TV camera 50, typically somewhere on the gantry. Another lens 48 receives the beam spot image at the output face of the light pipe 47 and converts the image into a beam of parallel light 49 which is thence directed through a narrow pass filter 51 having a pass band at the wavelength of the laser beam 22 so as to filter out undesired background illumination. The filtered beam is thence fed to a condensing lens 52 which focuses the beam spot image onto the receiving face of the TV camera 50. The input face of the light pipe 46 is cut at the Scheimpflug angle, as described in U.S. Pat. No. 751,347 issued Feb. 2, 1904, so that the plumb line 18 of the probe is maintained in focus on the input face of the TV camera 50.

Referring now to FIG. 5 there is shown, in block diagram form, the laser altimeter system 11 of the present invention. The output beam 22 of the laser 21 is fed through an optical distribution system 40 as shown in FIG. 3. One of the output beams 22 is selected and directed onto the terrain of the model 12 under the probe 14. The beam spot image 20 is picked up by both of the camera optical systems 30. Their output video signals are fed to a multiplexer 55. The computer 28 selects one or the other of the camera optic systems 30

and feeds a control signal to the multiplexer 55 for controlling which one of the camera optic systems 30 is utilized. The output of the multiplexer 55 is fed to the spot detector 26 which tracks the image of the beam spot 20 relative to the plumb line 18 which is inputted to the computer 28 and thence outputted to the motor driver 27 and respective motor 23. In a typical example, the computer 28 comprises a Motorola 6800 Exorcisor. The resolver 29 outputs the angle  $\theta$  for the selected beam 22 to an analog-to-digital converter in the computer 28. When the computer 28 detects zero error, i.e., the beam spot is at the plumb line 18, the computer 28 by its software looks up in a table the altitude corresponding to the respective angle  $\theta$  and outputs that data via a digital-to-analog converter to a driver 56 which thence inputs it to the altimeters or other read out devices 31.

Referring now to FIG. 6, there is shown the logic flow chart for the software program for the computer 28. FIGS. 7-9 depict the logic flow charts for program subroutines, namely, MOTOR MOVEMENT, DATA FETCH, and SCAN, respectively. The program listing is shown in Appendix I, below.

One of the advantages of the laser altimeter system of the present invention for a flight simulator includes detecting the altitude of the probe above a position directly below the probe as opposed to a position displaced in the horizontal plane from the probe. This makes the concept inherently accurate. Secondly, the provision of angularly displaced laser beams 22 and camera optics 30 allows reading of the altitude regardless of the obstructions represented by features in the terrain which might otherwise obstruct viewing of the beam spot.

## APPENDIX I

00010 00001				*****
00020 00002		*		LASER
00030 00003		*		OPERATING
00040 00004		*		SYSTEM
00050 00005		*****		*****
00060 00006			NAM	
00070 00007A 5000			ORG	\$5000
00080 00008			OPT	CRE, L, P=43, U, LLE=90
00090 00009A 5000	019F	A	CONV	FDB
00100 00010A 5002	04	A	SMMV	FCB
00110 00011A 5003	08	A	MDMV	FCB
00120 00012A 5004	10	A	LCMV	FCB
00130 00013A 5005	03CF	A	BIAS	FDB
00140 00014A 5007	ZF	EF41	A	CLR
00150 00015A 5008	ZF	EF43	A	CLR
00160 00016A 500D	ZF	EF51	A	CLR
00170 00017A 5010	ZF	EF53	A	CLR
00180 00018A 5013	ZF	EF40	A	CLR
00190 00019A 5016	ZF	EF42	A	CLR
00200 00020A 5019	ZF	EF50	A	CLR
00210 00021A 501C	B6	9C	A	LDAA
00220 00022A 501E	B7	EF52	A	STAA
00230 00023A 5021	B6	04	A	LDAA
00240 00024A 5023	B7	EF53	A	STAA
00250 00025A 5026	B7	EF43	A	STAA
00260 00026A 5029	ZF	EF52	A	CLR
00270 00027A 502C	B6	04	A	LDAA
00280 00028A 502E	B7	EF41	A	STAA
00290 00029A 5031	B7	EF51	A	STAA
00300 00030A 5034	B6	EF50	A	LDAA
00310 00031A 5037	B6	EF52	A	LDAA
00320 00032A 5034	B7	20	A	ANDA
00330 00033A 503C	Z7	0A	5040	REQ
00340 00034A 503E	B6	10	A	OUTOF
00350 00035A 5040	B7	EF52	A	LDAA
				*****
				CLR INTERRUPT
				INITIALIZE EVENT COUNTER
				##20
				BUFFER EMPTY?
				RAISE READ ENHANCE
				##10
				##FF52

00360 00036A 5043 7F EF52 A	CLR	\$EF52	
00370 00037A 5044 20 EF 5037	BRA	FLAG	RETURN, INITIAL DONE?
00380 00038A 5048 7F 533A A OUTLOP	CLR	STABLE	LINE STABILITY CHECK
00390 00039A 504B 7F 5339 A	CLR	STB1	* OF NO DOT PASSES
00400 00040A 504E 7F EF71 A	CLR	\$EF71	INITIALIZE MOTOR PIA
00410 00041A 5051 82 FF A	LDAA	\$FFF	
00420 00042A 5053 F2 EF70 A	STAA	\$EF70	
00430 00043A 5054 82 06 A	LDAA	\$6	
00440 00044A 5058 F2 EF71 A	STAA	\$EF71	
00450 00045A 505B BD 50A2 A GO	JSR	COLECT	GO GET DATA FROM VIDEO
00460 00046A 505E BD 525A A	JSR	DIST	GO CALC ALTITUDE
00470 00047A 5041 FE 53D4 A	LDX	DOT	
00480 00048A 5044 27 0A 5070	BEQ	STA1	IS DOT (NOT) THERE?
00490 00049A 5046 7F 5339 A	CLR	STB1	IF DOT, CLR * NO DOTS
00500 00050A 5069 8C 0001 A FILTER	CPX	\$1	
00510 00051A 504C 27 ED 505D	BEQ	GO	SYSTEM ERROR, TRY AGAIN
00520 00052A 504E 20 14 5084	BRA	RUN	RUN SYSTEM WITH GOOD DOT
00530 00053A 5070 86 01 A STA1	LDAA	\$1	* OF CONSEQ. NO DOT PASS
00540 00054A 5072 80 5339 A	SUBA	STB1	
00550 00055A 5075 27 05 507C	BEQ	SEND	NO DOT TWICE?
00560 00056A 5077 7C 5339 A	INC	STB1	ACK ONE NO DOT PASS
00570 00057A 507A 20 DF 505D	BRA	GO	
00580 00058A 507C 7F 5339 A SEND	CLR	STB1	CLR * OF NO DOT PASSES
00590 00059A 507F BD 5179 A	JSR	HUNT	GO HUNT FOR MISSING DOT
00600 00060A 5082 20 D7 505B	BRA	GO	RETURN AND TRY AGAIN
00610 00061A 5084 BC 5000 A RUN	CPX	CONV	RASTER LINE STAB. TEST
00620 00062A 5087 27 0C 5095	BEQ	SET1	CONVERGENT?
00630 00063A 5089 84 01 A	LDAA	\$1	PUT STABLE BIT HERE
00640 00064A 508B BD 533A A	SUBA	STABLE	
00650 00065A 508E 27 0D 509D	BEQ	DRIVE	IS DOT NOT CONV?
00660 00066A 5090 7C 533A A	INC	STABLE	ACK NOT CONV PASS
00670 00067A 5093 20 C6 505B	BRA	GO	RETURN AND TRY AGAIN
00680 00068A 5095 7F 533A A SET1	CLR	STABLE	
00690 00069A 5098 BD 525A A	JSR	DIST	CALC DIST FOR ALTIM
00700 00070A 509B 20 BE 505B	BRA	GO	RETURN AND PROCESS AGAIN
00710 00071A 509D BD 5200 A DRIVE	JSR	MOVE	GO TO MIRROR ADJUST SR.
00720 00072A 50A0 20 B9 505B	BRA	GO	RETURN AND REPROCESS
00730 00073A 50A2 7F 5359 A COLECT	CLR	LDATA	INITIALIZE DATA REG'S
00740 00074A 50A5 7F 535A A	CLR	LDATA+1	
00750 00075A 50AB 7F 5320 A	CLR	DDATA	
00760 00076A 50AB 2F 5396 A	CLR	DDATA+1	
00770 00077A 50AE 7F 53D1 A	CLR	COUNT1	
00780 00078A 50B1 7F 53D2 A	CLR	NUMB1	
00790 00079A 50B4 7F 53D5 A	CLR	COUNT2	
00800 00080A 50B7 B6 EF50 A	LDAA	\$EF50	CLR H-WARE INTERRUPT
00810 00081A 50B8 B6 80 A	LDAA	\$FF80	
00820 00082A 50B9 B7 EF52 A	STAA	\$EF52	START HARDWARE RUNNING
00830 00083A 50BF 86 FF A	LDAA	\$FFF	LOOP TIMER
00840 00084A 50C1 F6 EF51 A JMP2	LDAB	\$EF51	CHECK FOR DOT INTERRUPT
00850 00085A 50C4 21 39 50FF	BMI	READ	IF SEE DOT, READ DATA
00860 00086A 50C6 FF 53D3 A	STX	DUMMY	PAD LOOP TIME
00870 00087A 50C9 FF 53D3 A	STX	DUMMY	
00880 00088A 50CC FF 53D3 A	STX	DUMMY	
00890 00089A 50C9 FF 53D3 A	STX	DUMMY	
00900 00090A 50D2 FF 53D3 A	STX	DUMMY	
00910 00091A 50D5 FF 53D3 A	STX	DUMMY	
00920 00092A 50D8 FF 53D3 A	STX	DUMMY	
00930 00093A 50DB FF 53D3 A	STX	DUMMY	
00940 00094A 50DE FF 53D3 A	STX	DUMMY	
00950 00095A 50E1 FF 53D3 A	STX	DUMMY	
00960 00096A 50E4 FF 53D3 A	STX	DUMMY	
00970 00097A 50E7 FF 53D3 A	STX	DUMMY	
00980 00098A 50E9 FF 53D3 A	STX	DUMMY	
00990 00099A 50ED FF 53D3 A	STX	DUMMY	
01000 00100A 50F0 7C 53D1 A	INC	COUNT1	* OF NO DOT LOOPS
01010 00101A 50F3 B1 53D1 A	CMPA	COUNT1	\$FF LOOPS?
01020 00102A 50F6 26 C9 50C1	BNE	JMP2	RETURN AND TRY AGAIN
01030 00103A 50F8 CE 0000 A	LDX	\$0	
01040 00104A 50FB FF 53D4 A	STX	DOT	NO DOT FOUND
01050 00105A 50FE 39	RTS		RETURN TO MAIN FROG
01060 00106A 50FF 7F EF52 A READ	CLR	\$EF52	STOP HARDWARE SYSTEM
01070 00107A 5102 B6 EF52 A CHECK	LDAA	\$EF52	
01080 00108A 5105 84 20 A	ANDA	\$120	CHECK BUFFER NOT EMPTY
01090 00109A 5107 27 3A 5143	BEQ	DCENTR	ALL DATA IN, GET CNTR
01100 00110A 5109 83 10 A	LDAA	\$110	ENABLE READ ENABLE
01110 00111A 510B B7 EF52 A	STAA	\$EF52	
01120 00112A 510C B6 EF40 A	LDAA	\$EF40	GET WIDTH AND UNPACK
01130 00113A 5111 16	TAB		SAVE FOR FUTURE UNPACKING
01140 00113A 5112 B4 F0 A	ANDA	\$FF0	MASK OTHER INFO
01150 00115A 5114 34	LSRA		

01160 00116A 5115 44	LSRA		
01170 00117A 5116 44	LSRA		
01180 00118A 5117 81 03 A	CMFA	#\$	MINIMUM WIDTH
01190 00119A 5119 2F 23 513E	BLE	DISAB	IF TOO SMALL, SKIP
01200 00120A 511B 7D 53D5 A	TST	COUNT2	FIRSTGOODWIDTH?
01210 00121A 511E 26 1B 513B	BNE	JMP4	IF NOT, GO
01220 00122A 5120 B6 EF42 A	LDAA	#\$EF42	FIRST GOOD LINE
01230 00123A 5123 43	COMA		
01240 00124A 5124 B7 535A A MARK2	STAA	LDATA+1	STORE LSB OF RASTER LINE
01250 00125A 5127 17	TBA		
01260 00126A 5129 42	COMA		
01270 00127A 5129 84 01 A	ANDA	#\$1	
01280 00128A 5129 B/ 5352 A	STAA	LDATA	STORE MSB OF RASTER LINE
01290 00129A 512E D6 EF50 A	LDAA	#\$EF50	GET DISPLACEMENT DATA
01300 00130A 5131 B7 5396 A MARK3	STAA	DDATA+1	STORE LSB OF DISPLACEMENT
01310 00131A 5134 17	TBA		
01320 00132A 5135 B4 0E A	ANDA	#\$0E	
01330 00133A 5137 44	LSRA		
01340 00134A 5138 B7 5395 A	STAA	DDATA	
01350 00135A 513B 7C 53D5 A JMP4	INC	COUNT2	COUNT # OF GOOD DOTS
01360 00136A 513E 7F EF52 A DISAB	CLR	#\$EF52	DISABLE READ ENABLE
01370 00137A 5141 20 BF 5102	BRA	CHECK	
01380 00138A 5143 B6 53D5 A DCENTR	LDAA	COUNT2	# OF LINES WITH A DOT
01390 00139A 5146 B7 53DC A	STAA	WDCNT	
01400 00140A 5149 FE 5352 A	LDX	LDATA	GET FIRST LINE #
01410 00141A 514C FF 53D8 A	STX	LINE	
01420 00142A 514F FE 5395 A	LDX	DDATA	GET FIRST DISPLACEMENT
01430 00143A 5152 FF 530A A	STX	MAX	
01440 00144A 5155 74 53DC A	LSR	WDCNT	DIV BY TWO (FOR CENTER)
01450 00145A 5158 B6 53D9 A	LDAA	LINE+1	D.P. ADD FOR DOT CENTER
01460 00146A 515B B8 53DC A	ADDA	WDCNT	LSB ADD
01470 00147A 515E B7 53D7 A	STAA	DOT+1	STORE LSB
01480 00148A 5161 B6 53D8 A	LDAA	LINE	
01490 00149A 5164 82 00 A	ADCA	#\$0	MSB ADD
01500 00150A 5166 B7 53D6 A	STAA	DOT	MSB STORE
01510 00151A 5169 B6 53D7 A	LDAA	DOT+1	
01520 00152A 516C 84 01 A	ANDA	#\$1	TEST FOR ODDNESS
01530 00153A 516E 27 01 5171	BER	ADD1	ADD ONE IF EVEN
01540 00154A 5170 39	RTS		RETURN TO MAIN PROGRAM
01550 00155A 5171 FE 53D6 A ADD1.	LDX	DOT	ADD ONE TO MAKE ODD
01560 00156A 5174 08	INX		
01570 00157A 5175 FF 53D6 A	STX	DOT	
01580 00158A 5178 39	RTS		RETURN TO MAIN PROGRAM
01590 00159A 5179 CE 00FF A HUNT	LDX	#\$FF	
01600 00160A 517C FF 53D9 A	STX	INFIN	MIRROR AT INFINITE DIST
01610 00161A 517F CE FB54 A	LDX	#\$FB54	
01620 00162A 5182 FF 53D0 A	STX	ZERO	MIRROR AT ZERO DISTANCE
01630 00163A 5185 BD 50A2 A MZERO	JSR	COLECT	MOVE MIRROR TO ZERO
01640 00164A 5188 FE 53D6 A	LDX	DOT	CHECK IF A DOT WAS SEEN
01650 00165A 518B 26 72 51FF	BNE	JUMP	RETURN TO MAIN
01660 00166A 518D B6 EF08 A	LDAA	#\$EF08	
01670 00167A 5190 01	NOP		
01680 00168A 5191 FE EF08 A	LDX	#\$EF08	CHECK MIRROR POSITION
01690 00169A 5194 FF 53E1 A	STX	LOCA	STORE MIRROR LOCATION
01700 00170A 5197 B6 53E2 A	LDAA	LOCA+1	D.P. SUBTR-DIFF TO ZERO
01710 00171A 519A B6 53D6 A	SUPA	ZERO+1	LSB SUBTRACT
01720 00172A 519D B7 53E4 A	STAA	DTFF+1	LSB RESULT STORE
01730 00173A 51A0 B6 53E1 A	LDAA	LOCA	
01740 00174A 51A3 B2 53DD A	SECA	ZERO	MSB SUBTRACT
01750 00175A 51A6 B7 53E3 A	STAA	DIFF	STORE MSB RESULT
01760 00176A 51A9 FE 53E3 A	LDX	DIFF	
01770 00177A 51AC 2F 11 51FF	BLE	MINFIN	IF LT ZERO MOVE TO INFIN
01780 00178A 51AE 7F EF70 A	CLR	#\$EF70	OTHERWISE MOVE TO ZERO
01790 00179A 51B1 01	NOP		
01800 00180A 51B2 01	NOP		
01810 00181A 51B3 01	NOP		
01820 00182A 51B4 01	NOP		
01830 00183A 51B5 01	NOP		
01840 00184A 51B6 01	NOP		
01850 00185A 51B7 01	NOP		
01860 00186A 51B8 B4 0B A	LDAA	#\$0B	
01870 00187A 51BA B7 EF70 A	STAA	#\$EF70	MOVE MIRROR DOWN
01880 00188A 51BD 20 C6 5185	BRA	MZERO	
01890 00189A 51BF BD 50A2 A MINFIN	JSR	COLECT	LOOK FOR DOT
01900 00190A 51C2 FE 53D6 A	LDX	DOT	DOT THERE?
01910 00191A 51C5 26 38 51FF	BNE	JUMP	IF DOT THERE, RETURN
01920 00192A 51C7 B6 EF08 A	LDAA	#\$EF08	
01930 00193A 51CA 01	NOP		
01940 00194A 51CD FE EF08 A	LDX	#\$EF08	GET MIRROR POSITION

01950 00195A 51CE FF 53E1 A	STX	LOCA	STORE MIRROR LOCATION
01960 00196A 51D1 B6 53E2 A	LDAA	LOCA+1	D. P. SUBTR FOR DONE TEST
01970 00197A 51D4 B0 53E0 A	SUBA	INFIN+1	LSB SUBTRACT
01980 00198A 51D7 B7 53E4 A	STAA	DIFF+1	STORE LSB RESULT
01990 00199A 51DA B6 53E1 A	LDAA	LOCA	
02000 00200A 51DD B2 53DF A	SBCA	INFIN	MSB SUBTRACT
02010 00201A 51E0 B7 53E3 A	STAA	DIFF	STORE MSB RESULT
02020 00202A 51E3 FE 53E3 A	LDX	DIFF	CHECK IF DONE
02030 00203A 51E6 2C 11 51F9	BGE	DIE	IF NO DOT, DIE
02040 00204A 51E8 7F EF70 A	CLR	\$EF70	MOVE MIRROR TO INFINITY
02050 00205A 51EB 01	NOP		
02060 00206A 51EC 01	NOP		
02070 00207A 51ED 01	NOP		
02080 00208A 51EE 01	NOP		
02090 00209A 51EF 01	NOP		
02100 00210A 51F0 01	NOP		
02110 00211A 51F1 01	NOP		
02120 00212A 51F2 B6 AB A	LDAA	#\$AB	
02130 00213A 51F4 B7 EF70 A	STAA	\$EF70	MOVE MIRROR
02140 00214A 51F7 20 C6 51BF	BRA	MINFIN	RETURN AND LOOK FOR DOT
02150 00215A 51F9 86 3F A	DIE	LDAA	#\$3F
02160 00216A 51FB B7 51FE A	STAA	BK	
02170 00217A 51FE 01	BK	NOP	
02180 00218A 51FF 39	JUMP	RTS	
02190 00219	*****		
02200 00220	* MIRROR MOVE (ADJUST) SUBROUTINE *		
02210 00221	*****		
02220 00222A 5200 B6 5001 A	MOVE	LDAA	CONV+1 D. P. SUBTR FOR H.L. O. C.
02230 00223A 5203 B0 53D7 A		SUBA	DOT+1 L. O. C. =LINES OFF CENTER
02240 00224A 5206 B7 53F4 A		STAA	LOC+1 STORE LSB RESULT
02250 00225A 5209 B6 5000 A		LDAA	CONV
02260 00226A 520C B2 53D6 A		SECA	DOT MSB SUBTRACT
02270 00227A 520F B7 53F3 A		STAA	LOC STORE MSB RESULT
02280 00228A 5212 2F 53F5 A		CLR	MM CLEAR MOTOR MOVEMENT VAR
02290 00229A 5215 FE 53F3 A		LDX	LOC
02300 00230A 5218 27 3F 5259		BEQ	GOBCK NO MOVE IF CONVERGENT
02310 00231A 521A B0 01A0 A		CPX	#\$1A0
02320 00232A 521D 27 3A 5259		BEQ	GOBCK SYSTEM ERROR FILTER
02330 00233A 521F FE 53F3 A		LDX	LOC GET LOC FOR BRANCH
02340 00234A 5222 2B 1B 530F		BMI	MVUP IF LOC NEG., MOVE DOT UP
02350 00235A 5224 B6 20 A	MVDN	LDAA	#\$20
02360 00236A 5226 B7 53F5 A		STAA	MM
02370 00237A 5229 B0 53FE A		JSR	CLCMV
02380 00238A 522C 7F EF70 A		CLR	\$EF70
02390 00239A 522F 01		NOP	
02400 00240A 5230 01		NOP	
02410 00241A 5231 01		NOP	
02420 00242A 5232 01		NOP	
02430 00243A 5233 01		NOP	
02440 00244A 5234 01		NOP	
02450 00245A 5235 01		NOP	
02460 00246A 5236 B6 53F5 A		LDAA	MM GET MOTOR MOVEMENT
02470 00247A 5239 B7 EF70 A		STAA	\$EF70
02480 00248A 523C 2E 5259 A		JMP	GOBCK RETURN TO MAIN PROG
02490 00249A 523F B6 53F4 A	MVUP	LDAA	LOC+1
02500 00250A 5242 40		NEGA	
02510 00251A 5243 B7 53F4 A		STAA	LOC+1 ABSOLUTE VALUE OF LOC
02520 00252A 5246 B0 53FE A		JSR	CLCMV
02530 00253A 5249 7F EF70 A		CLR	\$EF70
02540 00254A 524C 01		NOP	
02550 00255A 524D 01		NOP	
02560 00256A 524E 01		NOP	
02570 00257A 524F 01		NOP	
02580 00258A 5250 01		NOP	
02590 00259A 5251 01		NOP	
02600 00260A 5252 01		NOP	
02610 00261A 5253 B6 53F5 A		LDAA	MM GET MOTOR MOVEMENT
02620 00262A 5256 B7 EF70 A		STAA	\$EF70 STORE IN MOTOR PIA
02630 00263A 5259 39	GOBCK	RTS	
02640 00264A 525A B6 EF08 A	DIIST	LDAA	\$EF08
02650 00265A 525D 01		NOP	
02660 00266A 525F FE EF08 A		LDX	\$EF08 GET MIRROR VOLTAGE
02670 00267A 5261 FF 53EF A		STX	MIRAD STORE IN MIRROR A/D
02680 00268A 5264 B6 53F0 A		LDAA	MIRAD+1 D. P. ADD- MIRROR A/D PLUS
02690 00269A 5267 B8 FF A		ADDA	#\$FF \$3FF (BIAS FOR TABLE)
02700 00270A 5269 B7 53F2 A		STAA	TOFSET+1 STORE LSB IN TABLE OFFSET
02710 00271A 526C B6 53EF A		LDAA	MIRAD
02720 00272A 526F B9 03 A		ADCA	#\$3 MSB ADD
02730 00273A 5271 B7 53F1 A		STAA	TOFSET STORE MSB IN TABLE OFFSET

02740	00274A	5274	B4	53F2	A	LDAA	TOFSET+1	MULTATABLEROFFSETBYWTWO
02750	00275A	5277	B8	53F2	A	ADDA	TOFSET+1	FOR D. P. DATA
02760	00276A	527A	B7	53F2	A	STAA	TOFSET+1	STORE LSB
02770	00277A	527D	B6	53F1	A	LDAA	TOFSET	
02780	00278A	5280	B2	53F1	A	ADCA	TOFSET	ADD MSB
02790	00279A	5283	B7	53F1	A	STAA	TOFSET	STORE MSB
02800	00280A	5286	B6	53F1	A	LDAA	TOFSET	ADD IN TABLE INITIALIZE
02810	00281A	5289	B8	75	A	ADDA	#\$75	LOCATE TABLE AT \$7000
02820	00282A	528D	B7	53F1	A	STAA	TOFSET	STORE IN MSB
02830	00283A	528E	FE	53F1	A	LDX	TOFSET	GET TABLE OFFSET
02840	00284A	5291	FF	5225	A	STX	FLAG1+1	INJECT IN DATA RETR. LOCA
02850	00285A	5294	FE	7000	A	LDX	\$2000	GET OUTPUT DATA FROM TABLE
02860	00286A	5297	FF	50F6	A	STX	TEMP2	STORE TO DO BIAS & SCALE
02870	00287A	529A	FF	53E9	A	STX	ER1	STORE FOR ERROR CALC
02880	00288A	529D	B4	53F7	A	LDAA	TEMP2+1	ADD LSP BIAS FACTOR
02890	00289A	52A0	BB	5006	A	ADDA	BIAS+1	LSB ADD
02900	00290A	52A3	B7	53F7	A	STAA	TEMP2+1	STORE BIASED LSB
02910	00291A	52A6	B4	53F6	A	LDAA	TEMP2	
02920	00292A	52A9	B9	5005	A	ADCA	BIAS	ADD MSB BIAS FACTOR
02930	00293A	52AC	B7	53F6	A	STAA	TEMP2	STORE BIASED MSB
02940	00294A					*	MULTIPLY BY 1.5 TO APPROX SCALE OUTPUT**	
02950	00295A	52AF	B6	53F6	A	LDAA	TEMP2	GET MSB OF VOLTAGE
02960	00296A	52B2	43			LSRA		DIVIDE BY 2
02970	00297A	52B3	B7	53F8	A	STAA	TEMP3	STORE MSB QUOTIENT
02980	00298A	52B4	B4	53F7	A	LDAA	TEMP2+1	GET LSB OF VOLTAGE
02990	00299A	52B9	46			RORA		DIVIDE BY 2 (PULL CARRY IN)
03000	00300A	52B4	B7	53F9	A	STAA	TEMP3+1	STORE LSB QUOTIENT
03010	00301A	52BD	B4	53F7	A	LDAA	TEMP2+1	ADD FOR 1.5 SCALE FACTOR
03020	00302A	52C0	BB	53F9	A	ADDA	TEMP3+1	LSB ADD
03030	00303A	52C3	B7	53FB	A	STAA	INSOUT+1	STORE LSB OF ALTIM OUTPUT
03040	00304A	52C6	B4	53F8	A	LDAA	TEMP3	
03050	00305A	52C9	B9	53F6	A	ADCA	TEMP2	MSB ADD
03060	00306A	52C0	B7	53FA	A	STAA	INSOUT	STORE MSB OF ALTIM OUTPUT
03070	00307A	52CF	FE	53FA	A	LDX	INSOUT	GET BIASED AND SCALED VALUE
03080	00308A	52D2	FF	EF20	A	STX	\$EF20	DO D/A CONV FOR ALTIM OUTPUT
03090	00309A	52D5	FE	53E9	A	LDX	ER1	GET ORIG TABLE VALUE
03100	00310A	52D8	FF	EF24	A	STX	\$EF24	DO D/A FOR STRIP CHART
03110	00311A	52FB	B4	EF0C	A	LDAA	\$EF0C	
03120	00312A	52DE	01			NOP		
03130	00313A	52DF	FE	EF0C	A	LDX	\$EF0C	GET TRACK VOLTAGE
03140	00314A	52E2	FF	53EB	A	STX	ER2	STORE FOR ERROR CALC
03150	00315A	52E5	B4	53FA	A	LDAA	ER1+1	D. P. SUBTR FOR ERROR CALC
03160	00316A	52LB	B0	53EC	A	SUBA	ER2+1	LSB SUBTR
03170	00317A	521B	B7	53E6	A	STAA	ERROR+1	LSB ERROR
03180	00318A	521E	B6	53C9	A	LDAA	ER1	
03190	00319A	521F	B2	53EB	A	SBCA	ER2	MSB SUBTRACT
03200	00320A	5214	B7	53ED	A	STAA	ERROR	MSB ERROR
03210	00321A	5217	FE	53ED	A	LDX	ERROR	GET FINAL ERROR VALUE
03220	00322A	521A	FF	EF22	A	STX	\$EF22	DO D/A FOR STRIP CHART
03230	00323A	521D	39			RTS		
03240	00324A	521E	B4	53F4	A	CLCMV	LDC+1	
03250	00325A	5301	B1	5002	A	CMFA	SMMV	MAKE A SMALL MOV'T?
03260	00326A	5304	2D	27	532D	BLT	SMALL	
03270	00327A	5306	B1	5003	A	CMPA	MDMV	MAKE A MEDIUM MOV'T?
03280	00328A	5309	2D	13	5323	BLT	MED	
03290	00329A	530B	B1	5004	A	CMPA	LCMV	MAKE A LARGE MOV'T?
03300	00330A	530E	2D	0A	531A	BLT	LARGE	
03310	00331A	5310	B4	84	A	LCST	#\$84	LARGEST POSS MOV'T
03320	00332A	5312	F4	53F5	A	LDAB	MM	GET DIRECTION
03330	00333A	5315	1B			ABA		COMBINE
03340	00334A	5316	B7	53F5	A	STAA	MM	STORE COMPLETED MOV'T
03350	00335A	531Y	39			RTS		
03360	00336A	531A	B4	83	A	LARGE	#\$83	LARGE MOV'T
03370	00337A	531C	F4	53F5	A	LDAB	MM	GET DIRECTION
03380	00338A	531F	1B			ABA		COMBINE
03390	00339A	5320	B7	53F5	A	STAA	MM	STORE COMPLETED MM
03400	00340A	5323	B6	82	A	MED	#\$82	MEDIUM MOV'T
03410	00341A	5325	F4	53F5	A	LDAB	MM	GET DIRECTION
03420	00342A	5328	1B			ABA		COMBINE
03430	00343A	5329	B7	53F5	A	STAA	MM	STORE MOTOR MOV'T
03440	00344A	532C	39			RTS		
03450	00345A	532D	B4	81	A	SMALL	#\$81	SMALLEST POSS MOV'T
03460	00346A	532F	F4	53F5	A	LDAB	MM	GET DIRECTION
03470	00347A	5332	1B			ABA		COMBINE
03480	00348A	5333	B7	53F5	A	STAA	MM	STORE MOV'T
03490	00349A	5336	39			RTS		
03500	00350A	5337	0002	A	VARI	RMB	2	† OF NO DOT PASSES
03510	00351A	5339	0001	A	STE1	RMB	1	† OF LINE STABLE PASSES
03520	00352A	533A	0001	A	STABLE	RMB	1	† OF LINE STABLE PASSES

03530 00353A 533B	001E	A	WDATA	RMB	30	WIDTH OF DOT DATA
03540 00354A 5359	003C	A	LDATA	RMB	60	RASTER LINE # DATA
03550 00355A 5395	003C	A	DDATA	RMB	60	DISPLACEMENT DATA
03560 00356A 53D1	0001	A	COUNT1	RMB	1	* OF COLLECT PASSES
03570 00357A 53D2	0001	A	NUMB1	RMB	1	
03580 00358A 53D3	0002	A	DUMMY	RMB	2	DUMMY TIME PAD VAR.
03590 00359A 53D5	0001	A	COUNT2	RMB	1	* OF LINES WITH A GOOD DOT
03600 00360A 53D6	0002	A	DOT	RMB	2	LOCATION OF DOT CENTER
03610 00361A 53D8	0002	A	LINE	RMB	2	TEMP STORE FOR DOT CENTER
03620 00362A 53DA	0002	A	MAX	RMB	2	SAME AS ABOVE
03630 00363A 53DC	0001	A	WDCT	RMB	1	
03640 00364A 53DD	0002	A	ZERO	RMB	2	* OF LINES W/ A GOOD DOT
03650 00365A 53DF	0002	A	INFIN	RMB	2	MIRROR VOLTAGE @ DIST=0
03660 00366A 53E1	0002	A	LOCA	RMB	2	MIRROR VOLTAGE @ D=INFIN
03670 00367A 53E3	0002	A	DIFF	RMB	2	CURRENT VOLTAGE OF MIRROR
03680 00368A 53E5	0002	A	TEMP1	RMB	2	DIFF BETW LOCA AND GOAL
03690 00369A 53E7	0002	A	TADD	RMB	2	TEMP REG FOR MOV'T CALC
03700 00370A 53E9	0002	A	ER1	RMB	2	TABLE ADDRESS
03710 00371A 53EB	0002	A	ER2	RMB	2	SYSTEM ERROR VAR 1
03720 00372A 53ED	0002	A	ERROR	RMB	2	SYSTEM ERROR VAR 2
03730 00373A 53EF	0002	A	MIKAD	RMB	2	RESULTANT SYSTEM ERROR
03740 00374A 53F1	0002	A	TOFSSET	RMB	2	MIRROR VOLTAGE FOR DIST
03750 00375A 53F3	0002	A	LOC	RMB	2	TABLE OFFSET (BIAS)
03760 00376A 53F5	0001	A	MM	RMB	1	* OF LINES OFF CONVERGE
03770 00377A 53F6	0002	A	TEMP2	RMB	2	MOTOR MOVEMENT
03780 00378A 53F8	0002	A	TEMP3	RMB	2	TEMP REG FOR DIST CALC
03790 00379A 53FA	0002	A	INSOUT	RMB	2	TEMP REG FOR DIST CALC
03800 00380A 53FC 39			RETU	RTS		ALTIMETER OUTPUT VOLTAGE
03810 00381			END			

TOTAL ERRORS 00000--00000

5171 ADD1	00153	00155*										
5005 BIAS	00013*	00289	00292									
51FE BK	00216	00217*										
5102 CHECK	00107*	00137										
52FE CLCMV	00237	00252	00324*									
50A2 COLECT	00045	000/3*00143	00189									
5000 CONV	00009*	00061	00222	00225								
53D1 COUNT1	00077	00100	00101	00356*								
53D5 COUNT2	00079	00120	00135	00138	00359*							
5143 DCENTR	00109	00138*										
5395 DDATA	00075	00076	00130	00134	00142	00355*						
51F9 DIE	00203	00215*										
53E3 DIFF	00172	00175	00176	00198	00201	00202	00367*					
513E DISAE	00119	00136*										
525A DIST	00046	00069	00264*									
53D6 DOT	00047	00104	00147	00150	00151	00155	00157	00164	00190	00223	00226	00360*
509D DRIVE	00045	00071*										
53D3 DUMMY	00086	00087	00088	00089	00090	00091	00092	00093	00094	00095	00096	00097
00098	00099	00350*										
53E9 ER1	00282	00309	00315	00318	00370*							
53EB ER2	00314	00316	00319	00371*								
53ED ERROR	00317	00320	00321	00372*								
5069 FILTER	00050*											
5037 FLAG	00031*	00037										
5294 FLAG1	00284	00285*										
505B GO	00045*	00051	00057	00060	00067	00070	00072					
5259 GOBCK	00230	00232	00248	00263*								
5179 HUNT	00059	00159*										
53DF INFIN	00160	00197	00200	00365*								
53FA INSOUT	00303	00306	00307	00379*								
50C1 JMP2	00084*	00102										
513B JMP4	00121	00135*										
51FF JUMP	00165	00191	00218*									
531A LARGE	00330	00336*										
5359 LDATA	00073	00074	00124	00128	00140	00359*						
5004 LCMV	00012*	00329										
5310 LOST	00331*											
50D8 LINE	00141	00145	00148	00361*								
53F3 LOC	00224	00227	00229	00233	00249	00251	00324	00375*				
53E1 LOCA	00169	00170	00173	00195	00196	00199	00366*					
5124 MARK2	00124*											
5131 MARK3	00130*											
53DA MAX	00143	00362*										
5003 MDMV	00011*	00327										
5323 MED	00378	00346*										

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518F MINFIN 00177 00189*00214
53EF MIRAD 00267 00268 00271 00373*
53F5 MM 00228 00236 00246 00261 00332 00334 00337 00339 00341 00343 00346 00348
    00376*
5200 MOVE 00071 00222*
5224 MVDN 00235*
523F MVUP 00234 00249*
5185 MZERO 00163*00188
53D2 NUMB1 00078 00357*
5048 OUTLDP 00033 00038*
50FF READ 00085 00106*
53FC RETU 00380*
5084 RUN 00052 00061*
507C SEND 00055 00058*
5095 SET1 00062 00068*
532D SMALL 00326 00345*
5002 SMMV 00010*000325
5070 STA1 00048 00053*
533A STABLE 00038 00064 00066 00068 00352*
5339 STB1 00039 00049 00054 00056 00058 00351*
53E7 TADD 00369*
53E5 TEMP1 00368*
53F6 TEMP2 00286 00288 00290 00291 00293 00295 00298 00301 00305 00377*
53F8 TEMP3 00297 00300 00302 00304 00378*
53F1 TOFSET 00270 00273 00274 00275 00276 00277 00278 00279 00280 00282 00283 00374*
5337 VARI 00350*
5338 WDATA 00353*
53DC WDCNT 00139 00144 00146 00363*
53DD ZERO 00162 00171 00174 00364*

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I claim:

1. In a method for determining the altitude of a flight simulator probe moving relative to and above the terrain of a flight simulator model wherein the imaginary line extending from the probe in a direction normal to the model is characterized as the probe plumb line, the steps of:

30 directing a pencil-like beam of radiation from said probe onto the model keeping said beam within a plane containing said probe plumb line to produce a beam spot on said model;

35 detecting the location of said beam spot relative to two orthogonal coordinates with a detector situated remote from said probe plumb line and having a linear sensitivity zone optically aligned with said probe plumb line;

40 varying the angular orientation of the beam within said probe plumb line plane and relative to a reference plane so as to cause said beam spot to impinge on the model site intersected by said probe plumb line;

45 determining the angular orientation of the beam relative to said reference plane; and

utilizing the determined angular orientation of said beam to determine the altitude of said probe over the terrain of the model.

50 2. The method of claim 1 including the step of, directing a second beam of radiation onto the terrain of the model from a position on the probe angularly spaced from the position of the first beam taken about an axis of revolution generally coaxially of said probe plumb line; and detecting the second beam spot when said first beam spot is obstructed by the terrain from reaching the intersection of the model and the probe plumb line.

55 3. The method of claim 1 wherein said beam of radiation is a beam of monochromatic, collimated light.

4. The method of claim 1 wherein the step of detecting the beam spot includes the step of directing a beam spot image through a light pipe on a path between the beam spot and the detector.

5. The method of claim 2 wherein the step of directing the second beam of radiation onto the terrain includes the step of splitting off of the first beam a portion of its energy to produce said second beam.

6. In a flight simulator apparatus of the type where a probe simulates an aircraft and the simulator operator controls the motion of the probe relative to the terrain of a model while viewing said model via a video monitor on said probe:

means for directing a pencil-like beam of radiation from the probe onto the terrain of the model to produce a beam spot on the model where the beam impinges on the model, an imaginary line extending from said probe normal to said model being known as the probe plumb line;

means supported by said probe for detecting the location of said beam impingement on said model, said means being remote from said probe plumb line, being two-dimensionally sensitive, and having a linear sensitivity zone in optical alignment with said probe plumb line;

servo means coupled to said beam directing means and said detecting means for varying the angular direction of the beam in a plane containing the probe plumb line and maintaining the beam spot on the model at the site where the probe plumb line intersects the model;

means for determining the angular orientation of the beam relative to a reference plane; and

means for utilizing the determined angular orientation of said beam to determine the distance between said probe and said model measured along said probe plumb line.

7. The apparatus of claim 6 including:

means for directing a second beam of radiation onto the terrain of the model from a position on the probe angularly spaced from the position of the first beam taken about an axis of revolution generally coaxial of said probe plumb line; and

means for detecting the second beam spot when said first beam spot is obstructed by the terrain from

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reaching the model site intersected by the probe plumb line.

8. The apparatus of claim 6 wherein said means for directing a pencil-like beam of radiation includes means for directing a pencil-like beam of monochromatic, collimated light.

9. The apparatus of claim 6 including light pipe means

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for directing an image of said beam spot to said detecting means.

10. The apparatus of claim 7 including beam splitter means for splitting off a portion of said first beam to produce said second beam.

11. The apparatus of claim 6 wherein said detecting means includes a video camera.

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